



WIR SCHAFFEN WISSEN – HEUTE FÜR MORGEN

D. Rochman

# Nuclear data uncertainty propagation

## Part 3: ND Uncertainties for reactors and fuel.

EXTEND summer school, Uppsala University, Sweden, September 2<sup>nd</sup>, 2016



# Summary

- Applications to energy systems (*Part 3*)

## I. Methods: Monte Carlo (TMC) vs. perturbation (sensitivity)

## II. Results with TMC

1. Criticality-safety benchmarks
2. PWR Fuel pin keff
3. Assemblies
4. Full core
5. Transient

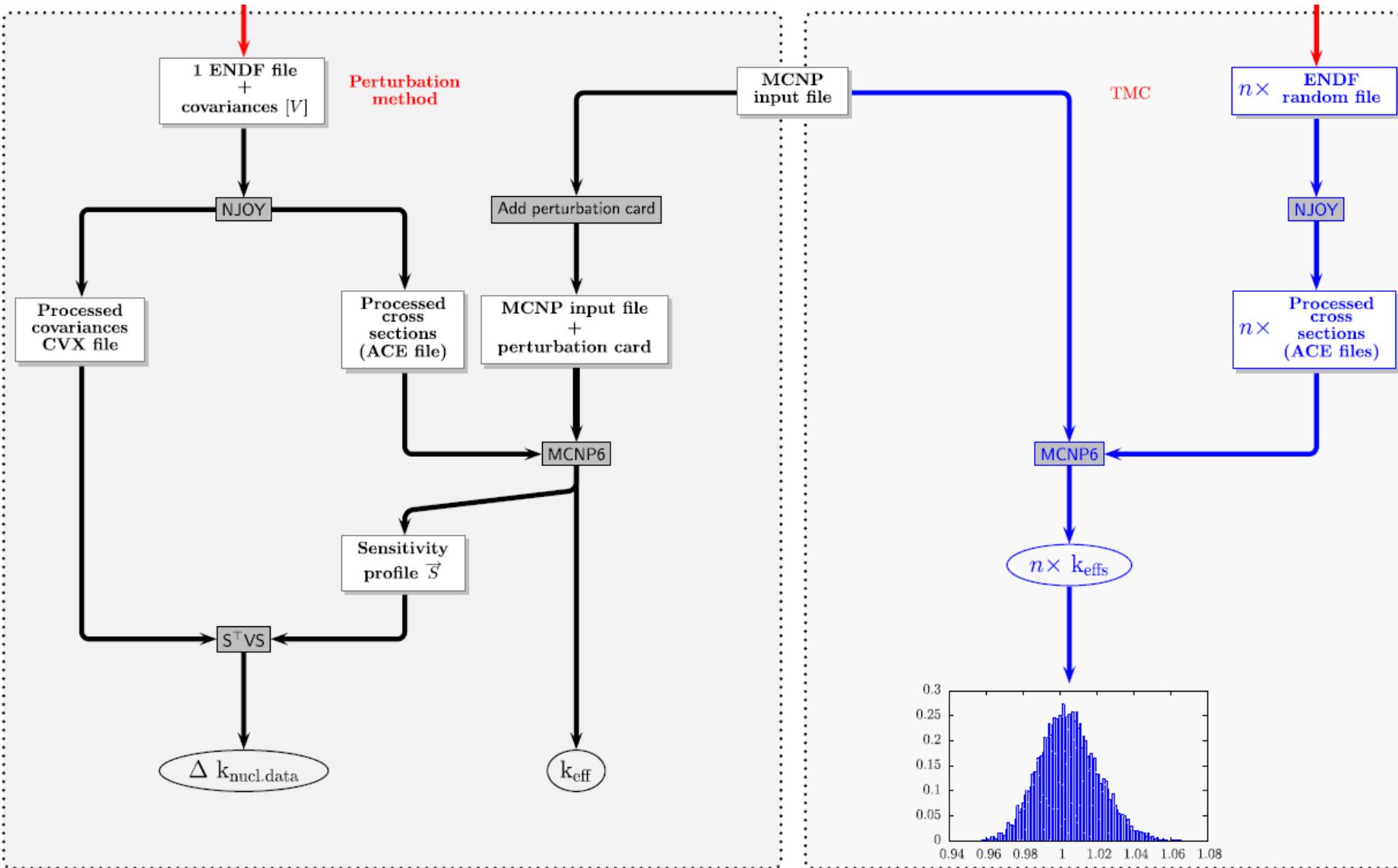
## III. Uncertainties from methods

## IV. Other uncertainties

All slides can be found here: [https://tendl.web.psi.ch/bib\\_rochman/presentation.html](https://tendl.web.psi.ch/bib_rochman/presentation.html)

# Methods

- As mentioned before, there are basically two ways of propagating uncertainties



# Methods

- In any case, uncertainties are not real quantities, contrary to cross sections
- They are only a reflection of the method applied and of the considered inputs !

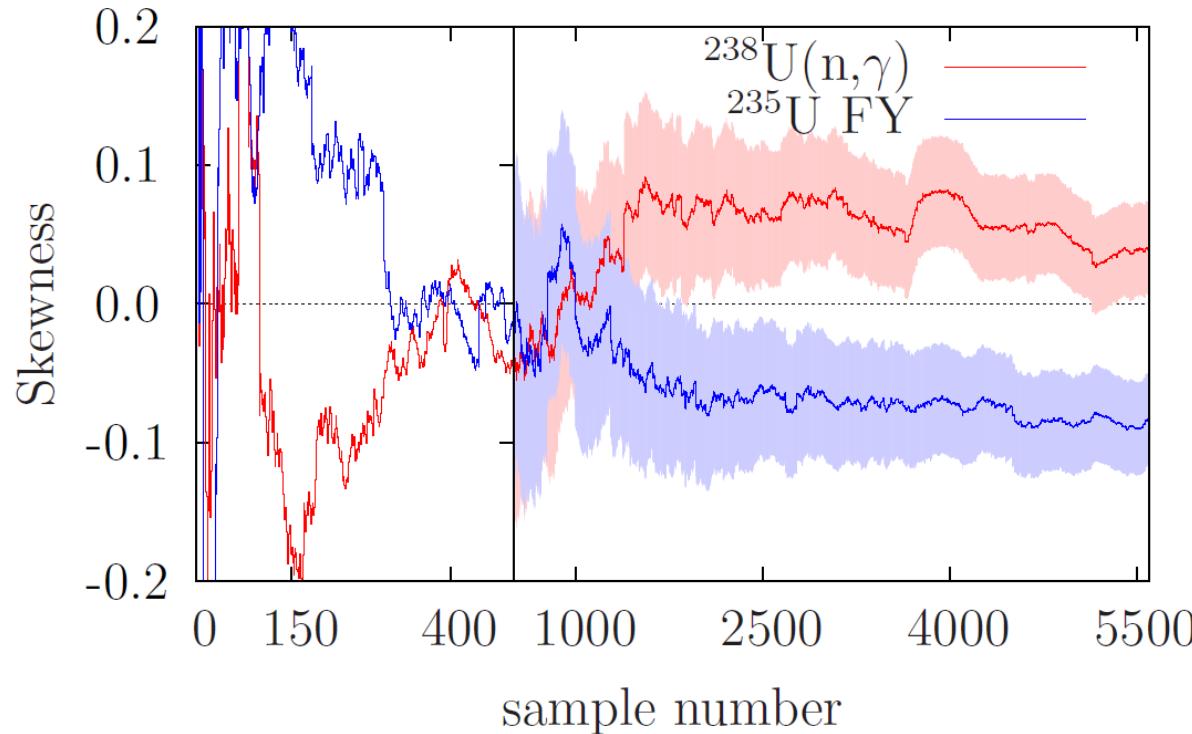
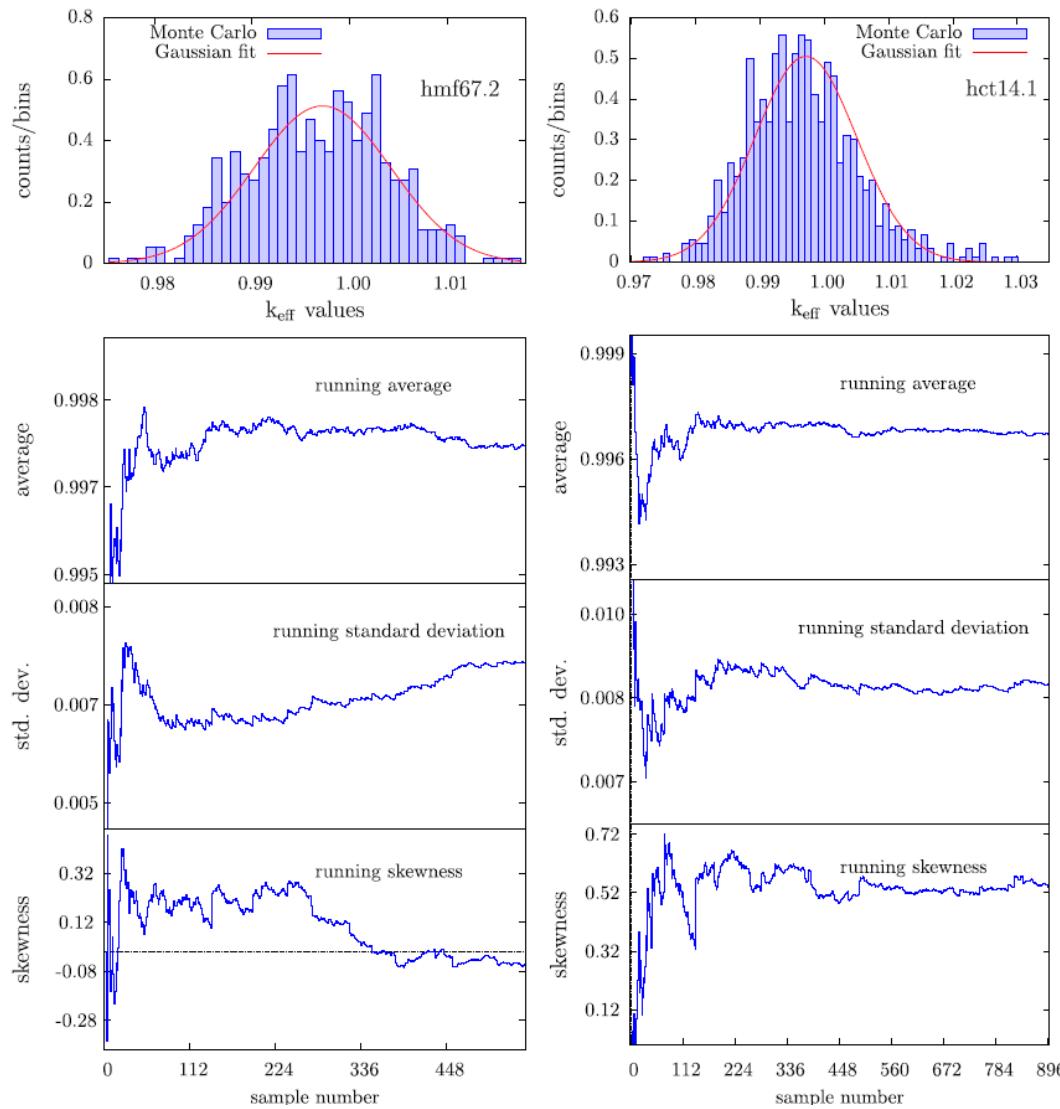


FIG. 46. (Color online) Examples of two different skewness for the same quantity, the number density of the pseudo fission product, changing the  $^{238}\text{U}(n,\gamma)$  cross section at 10 keV in one case (red) and the  $^{235}\text{U}$  fission yields in the other case (blue).

# Methods

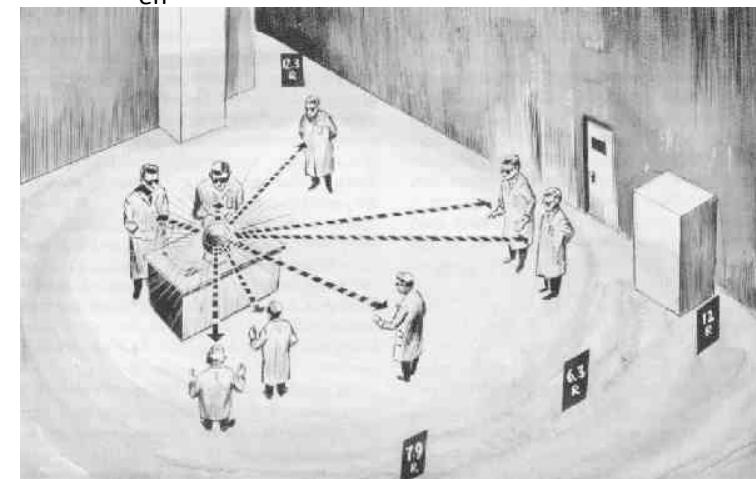
- In Monte Carlo method, the convergence of the results is a key quantity



# Results

## 1. Criticality-safety benchmarks

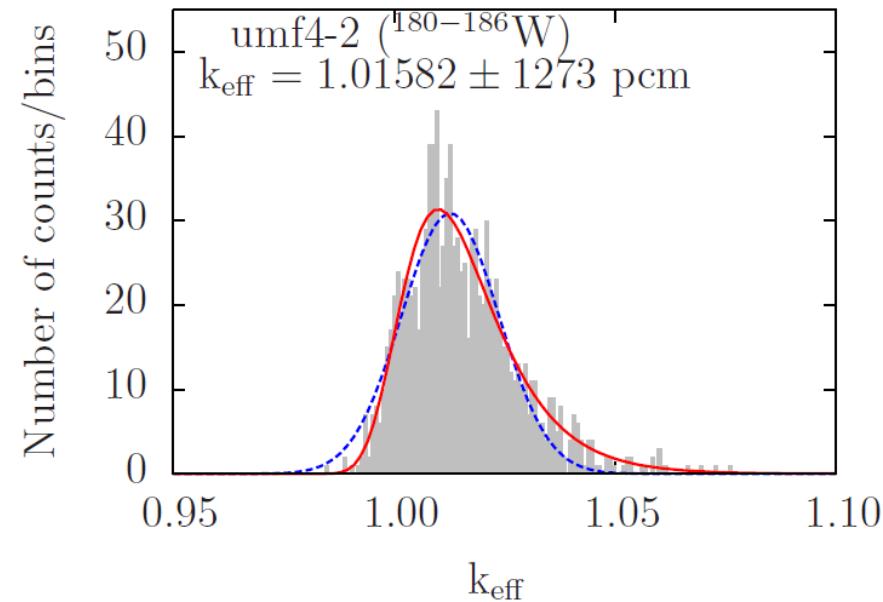
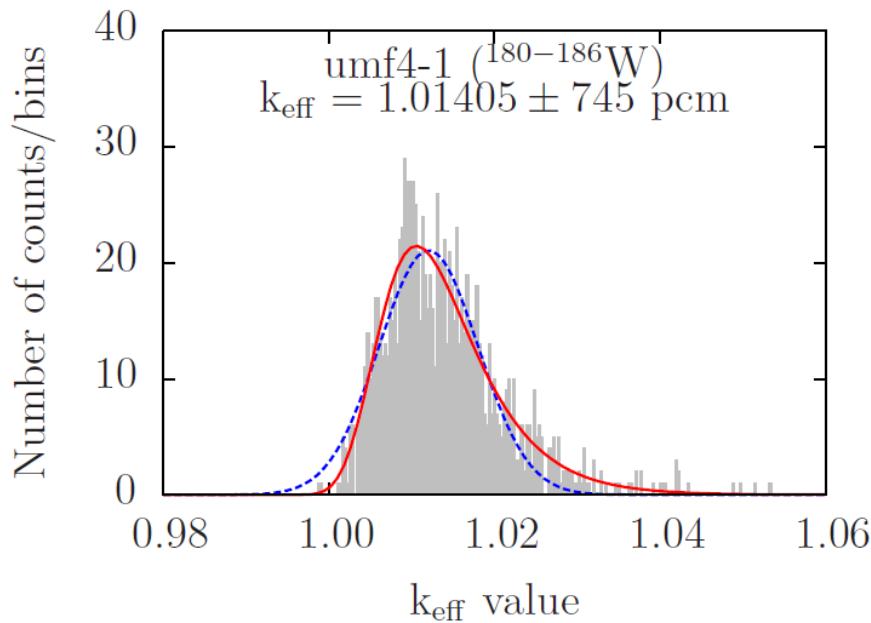
- Criticality-safety benchmarks are crucial to assess the criticality safety of nuclear installation (fuel storage, liquid waste, fissile material storage...)
- It is all about  $k_{\text{eff}}$  and must be  $< 1$
- Safety authorities often impose an administrative limit of 0.95 (**conservative** approach)
- Economics pushes for a “**best estimate + uncertainties**” approach
  - As a consequence, 0.95 might not be valid anymore,
  - As a consequence, more fissile material can be stored,
  - All depending on precise estimation of the uncertainties on  $k_{\text{eff}}$ .



# Results

## 1. Criticality-safety benchmarks

- Criticality benchmarks are used to validate codes (such as MCNP) to make sure that the calculated  $k_{\text{eff}}$  is correct.
- Additionally, Monte Carlo Uncertainty propagation method lead to “pdf”, more suitable for uncertainty-safety assessments



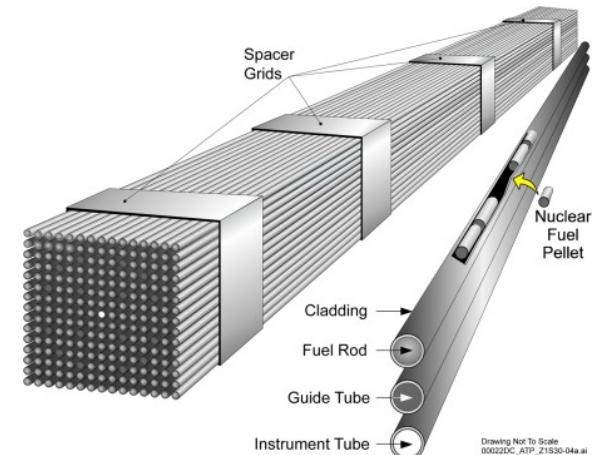
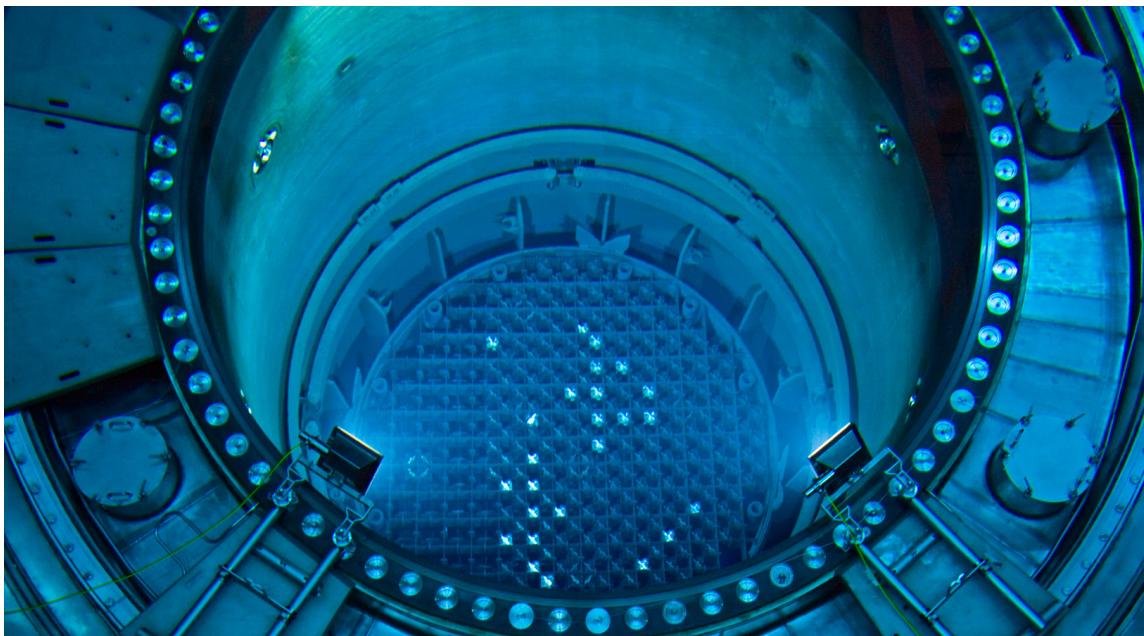
- The strength of the MC methods is in the access to the moments of the distributions, not reflected by a single number such as the standard deviation.

# Results

## 2. PWR Fuel pin

All starts with a pincell:

- **Assembly** simulations start with **pincell** simulations,
- **Core** simulations start with **assembly** simulations,
- Fuel storage simulations start **assembly** simulations,



# Results

## 2. PWR Fuel pin

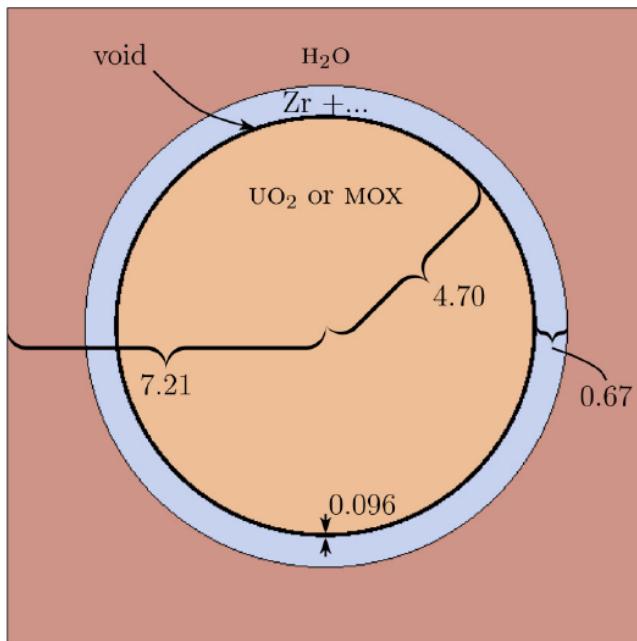


Fig. 1. The geometry of the pin cell model used in Serpent. The fuel, either  $\text{UO}_2$  or MOX, is surrounded by concentric annular rings with a void and Zircaloy clad. The rest of the square is filled with water, and all sides are subject to reflecting boundary conditions. All distances are in millimeters.

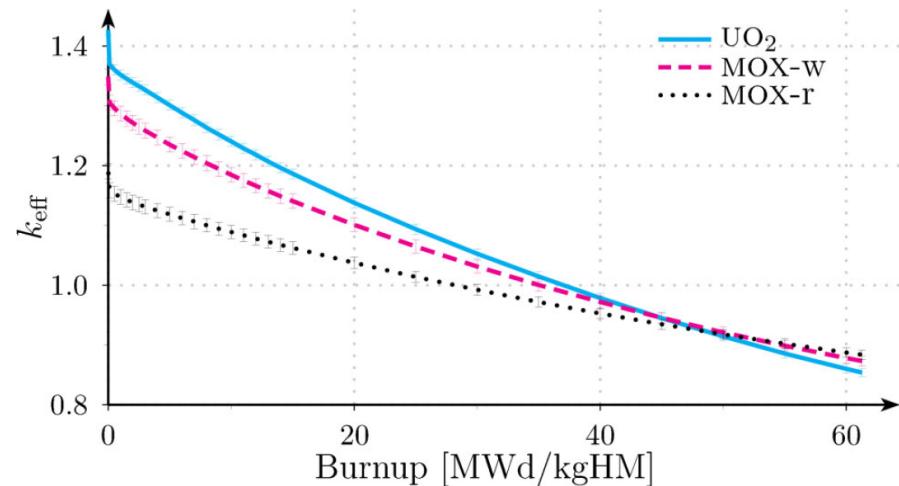


Fig. 3.  $k_{\text{eff}} = k_{\infty}$  as a function of burnup for the three fuel types. The large deviations from 1 are explained by the simplified model: no leakage, infinite grid of pin cells (with the same burnup), and no control mechanisms. The uncertainty bars represent the data uncertainty  $\sigma_{\text{data}}(k_{\text{eff}})$ ; the statistical uncertainty is negligible in comparison.

## Results

## 2. PWR Fuel pin

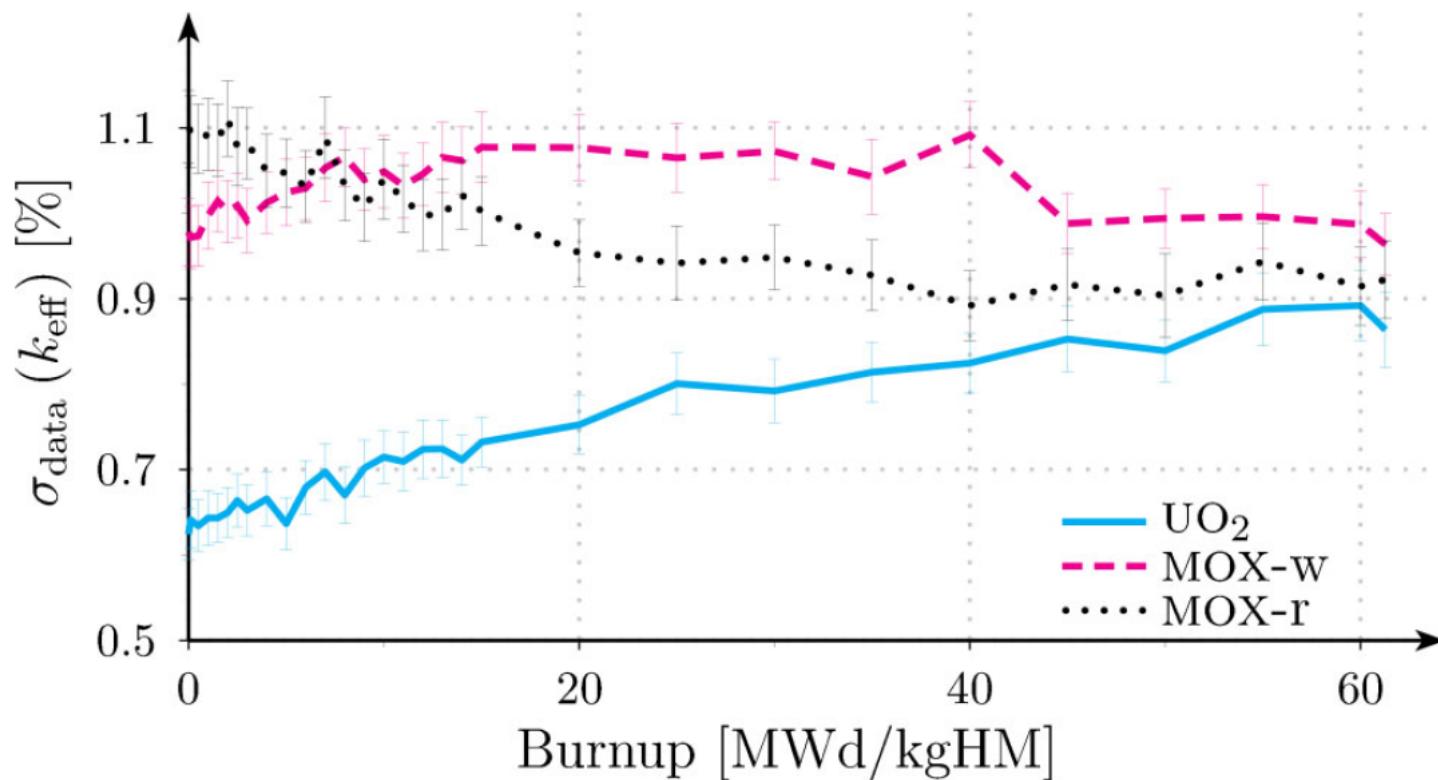


Fig. 2. The main result: Propagated data uncertainty in  $k_{\text{eff}}$  for  $\text{UO}_2$  and the two types of MOX fuel as functions of burnup due to all data. The uncertainty bars represent one standard deviation.

## Results

## 2. PWR Fuel pin

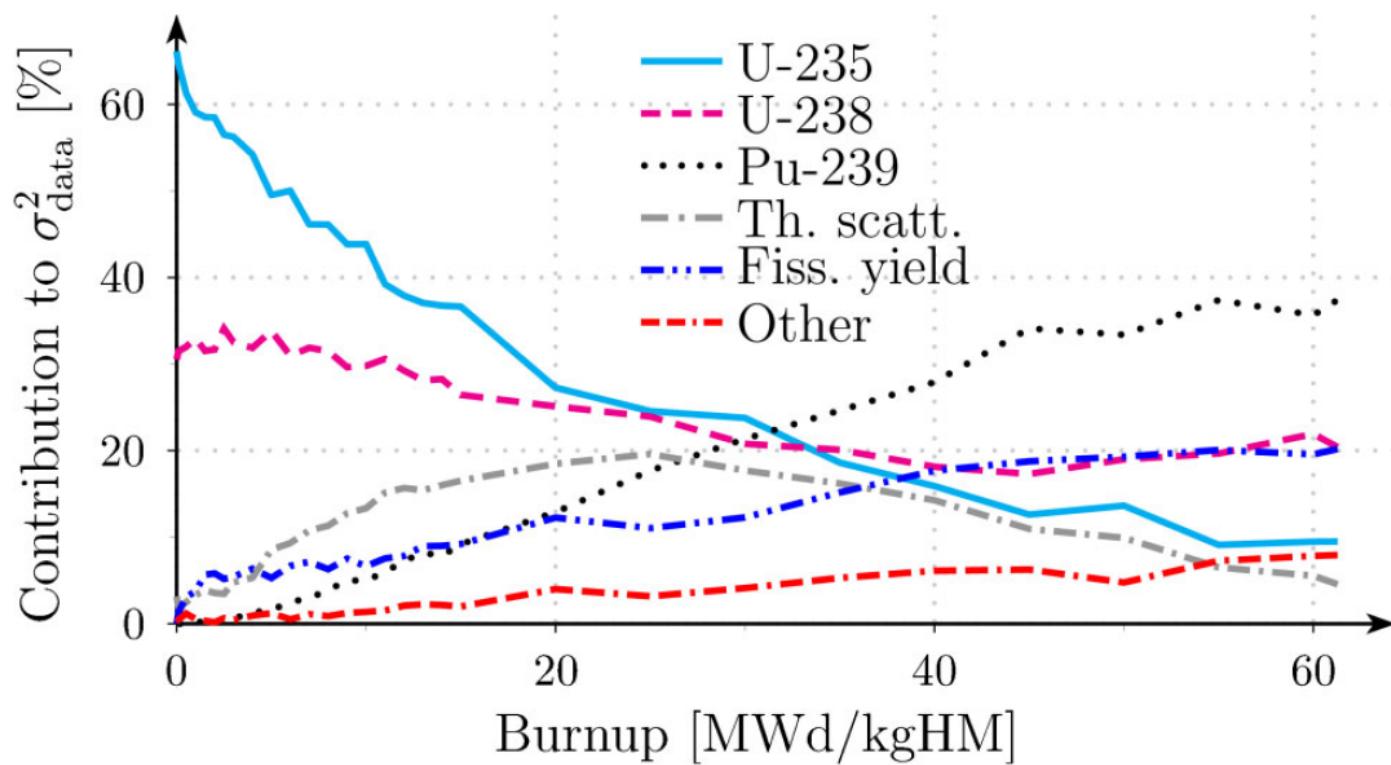


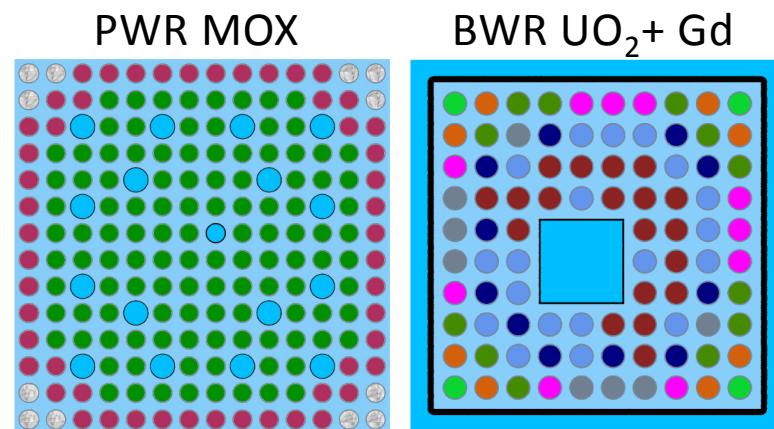
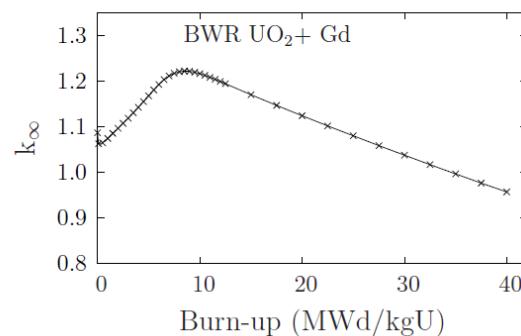
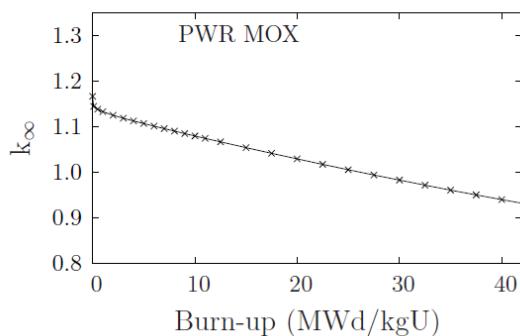
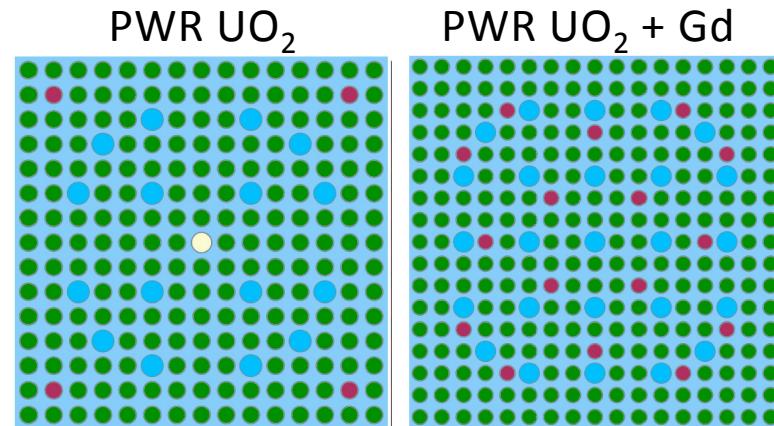
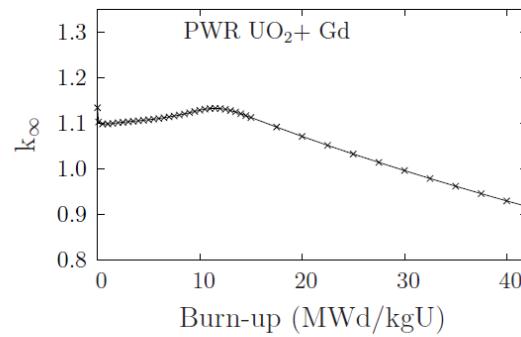
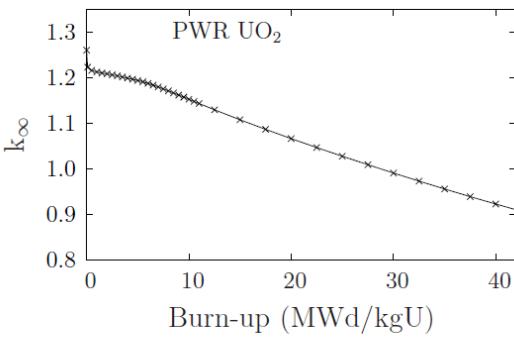
Fig. 4. Contributions to total variance in  $k_{\text{eff}}$  from variance of individually varied data, for  $\text{UO}_2$ . “Other” stands for transport and activation data of fission products and minor actinides.

# Results

## 3. Assembly

- Different types of assemblies exist: e.g. PWR, BWR, with  $\text{UO}_2$ , MOX

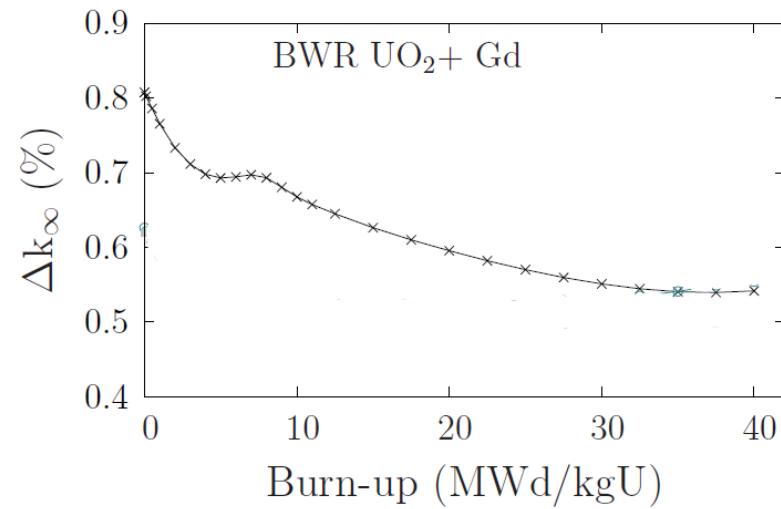
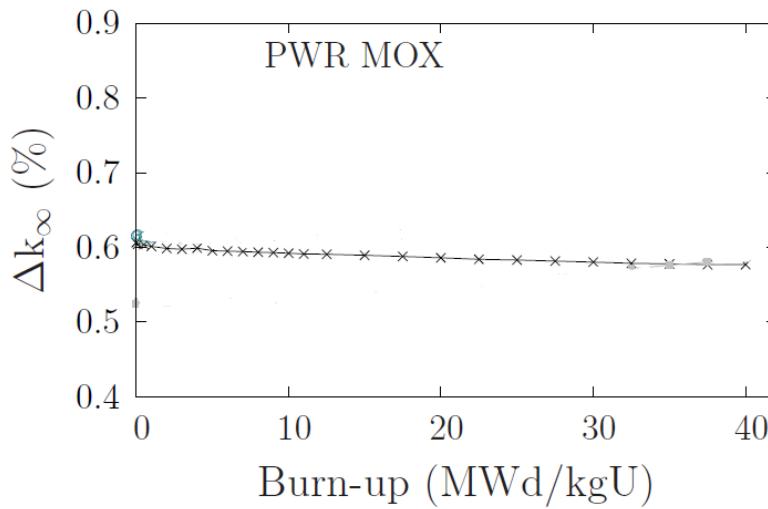
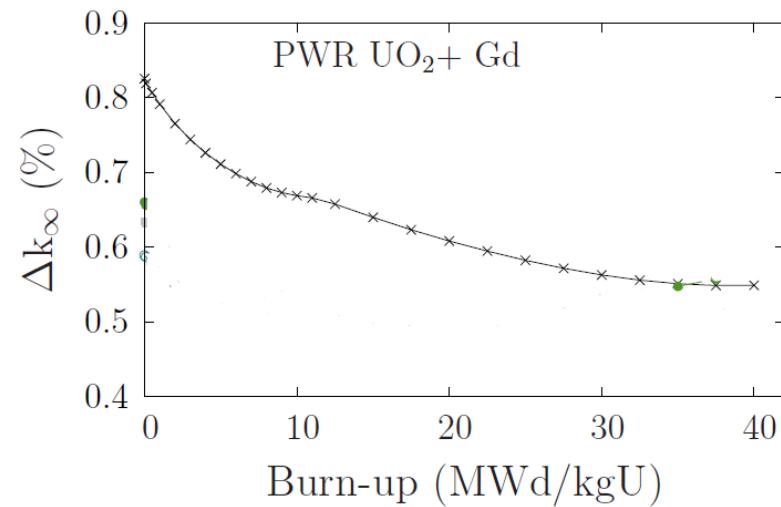
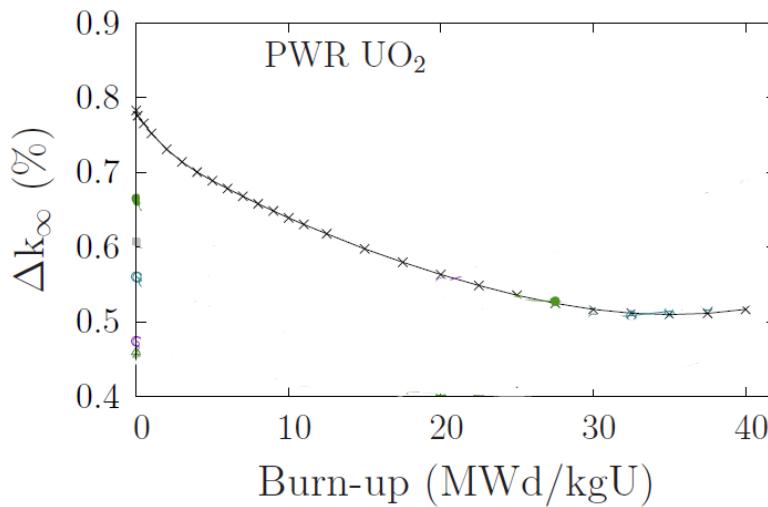
- It leads to different uncertainties
- Only 2D models are usually used



# Results

## 3. Assembly

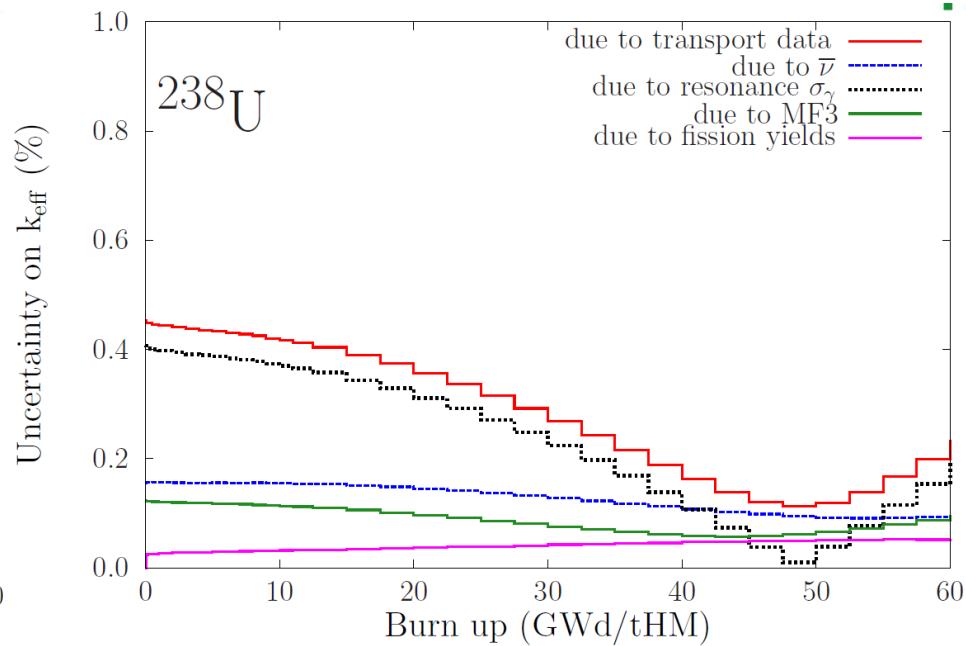
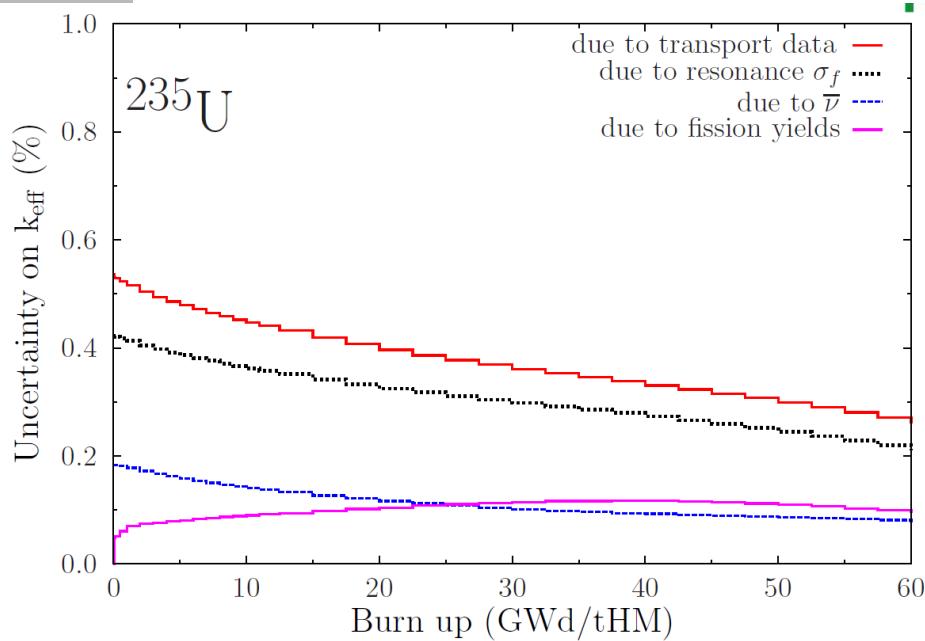
- $K_{inf}$  uncertainty for 4 assemblies, 1 reactor cycle



# Results

## 3. Assembly

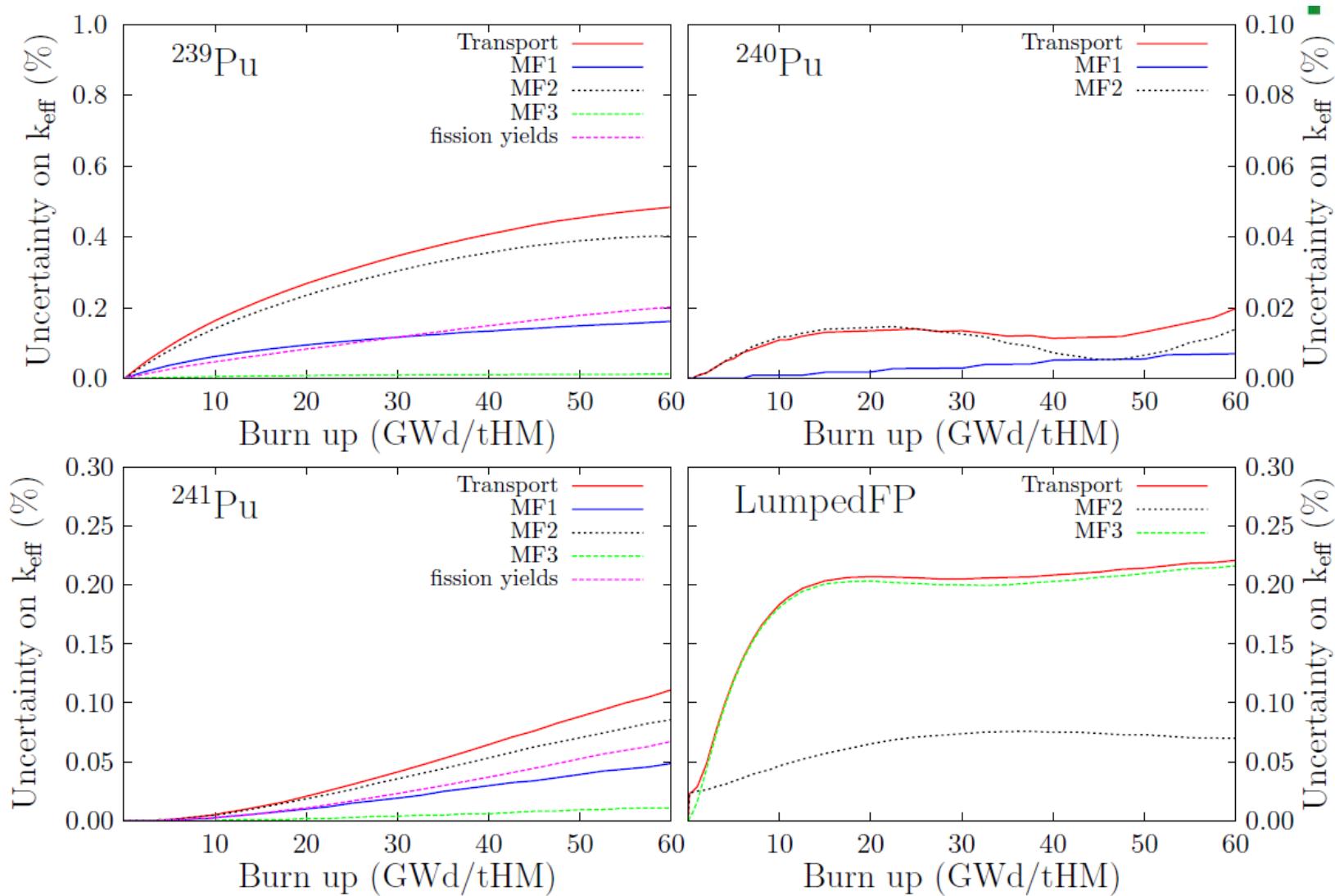
- $K_{inf}$  uncertainty contributions



# Results

## 3. Assembly

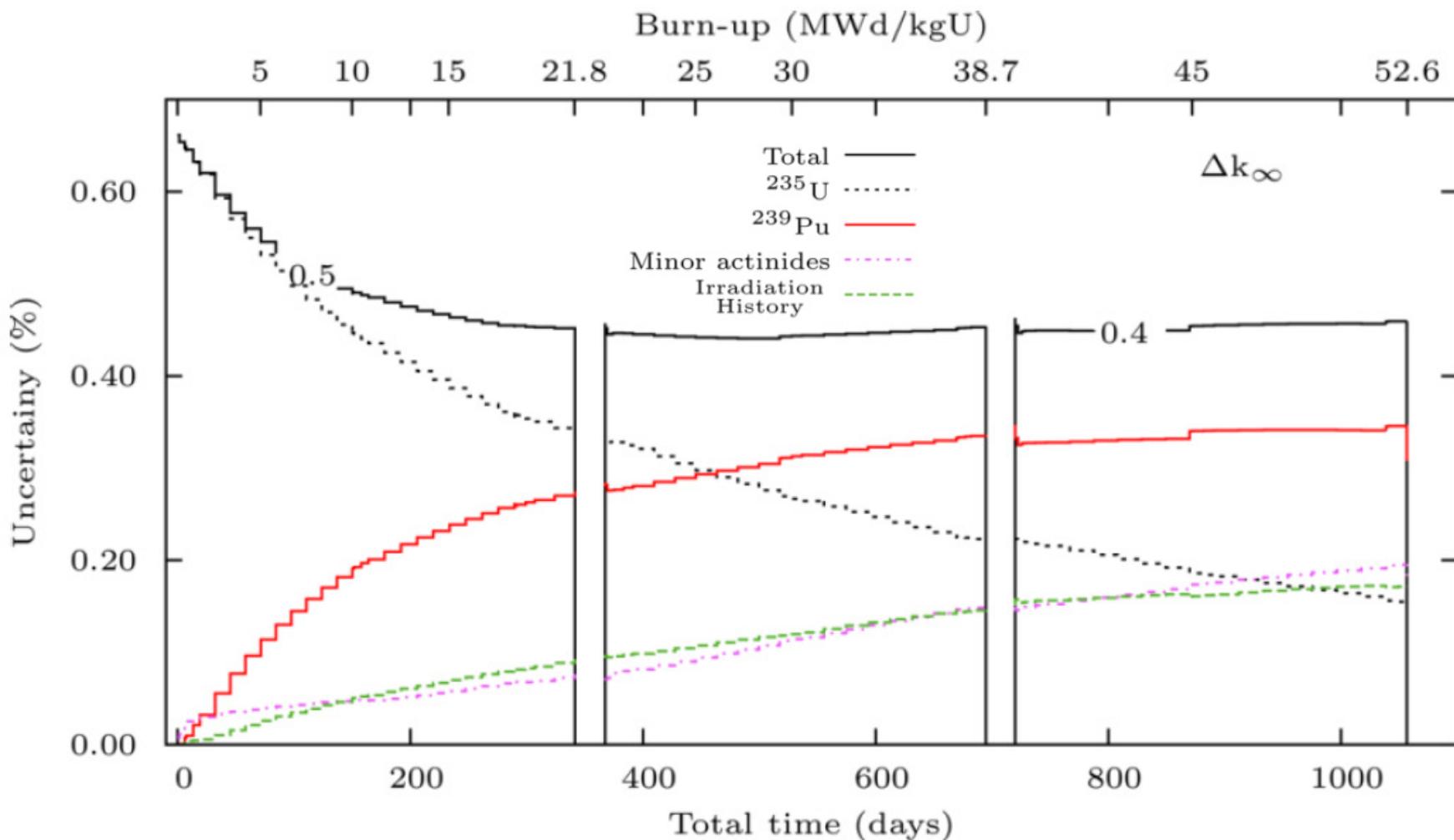
- $K_{inf}$  uncertainty contributions



# Results

## 3. Assembly

- $K_{inf}$  uncertainty for a PWR  $\text{UO}_2$ , over 3 successive reactor cycles



# Results

## 4. Full core

- Uncertainty at different locations due to nuclear data,
- For different quantities (inventory, boron concentration, power distribution, safety parameters such as Linear Heat Generation rate...)
- No sensitivity method can be applied

CYCLE MOX

	1	2	3	4	5	6	7	8	9	10	11	12	13	
A						29	34	30						
B				30	0	0 *	10	0 *	0	27				
C			30	0	8 *	32	6	32	8 *	0	30			
D		27	0	15	19	9	30	9	19	15	0	30		
E		0	8 *	19	17 *	29	10 *	28	17 *	19	8 *	0		
F	30	0 *	32	9	28	10	17	10	29	9	32	0 *	29	
G	34	10	6	30	10 *	17	27 *	17	10 *	30	6	10	34	
H	29	0 *	32	9	29	10	17	10	28	9	32	0 *	30	
I		0	8 *	19	17 *	28	10 *	29	17 *	19	8 *	0		
J		30	0	15	19	9	30	9	19	15	0	27		
K			30	0	8 *	32	6	32	8 *	0	30			
L				27	0	0 *	10	0 *	0	30				
M					30	34	29							

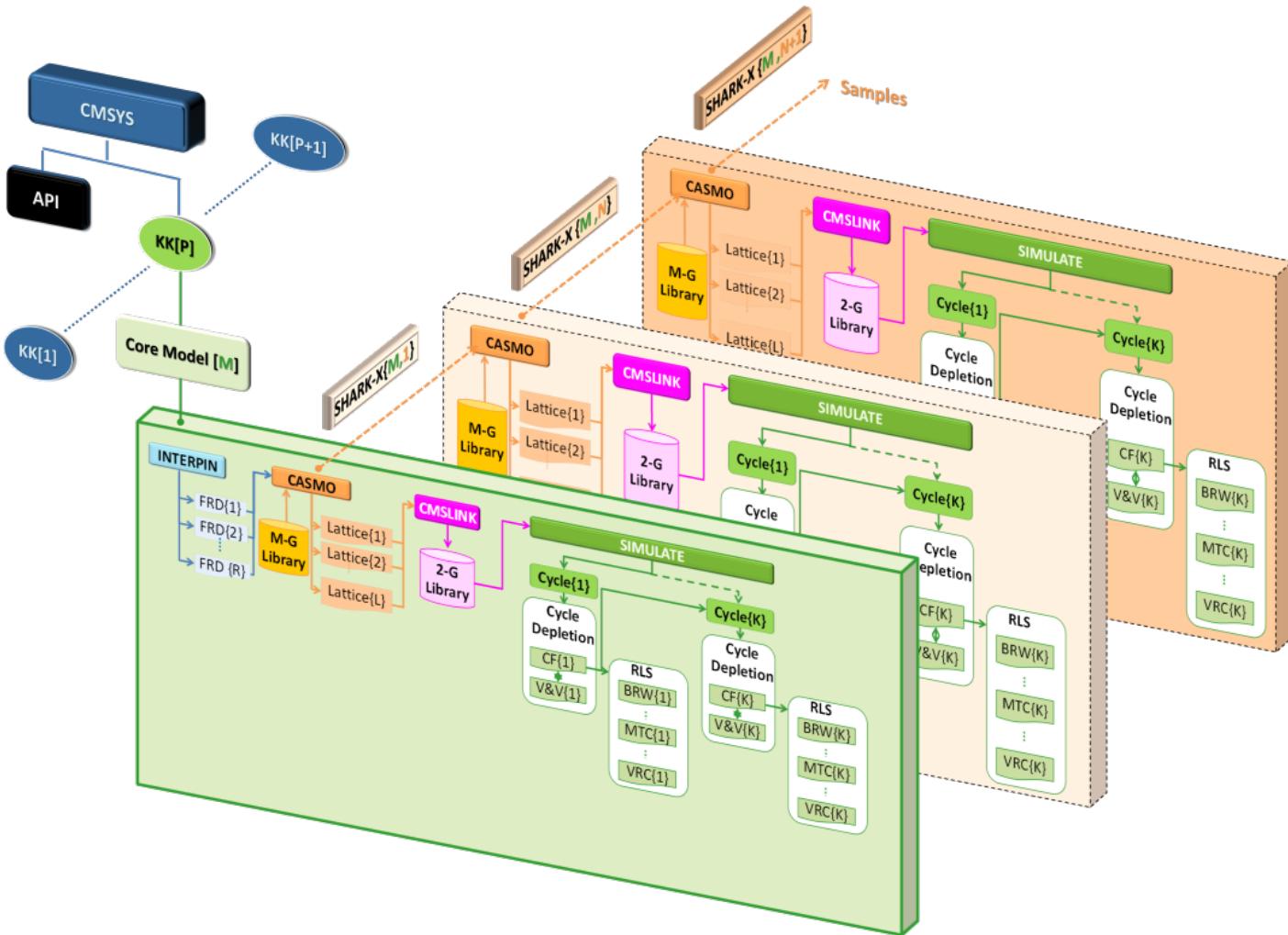
CYCLE UOX

	1	2	3	4	5	6	7	8	9	10	11	12	13	
A						57	55	57						
B				47	38	0 *	0	0 *	37	47				
C			55	0	11 *	47	51	47	11 *	0	55			
D		47	0	37	36	11	38	11	36	37	0	47		
E		37	11 *	36	25 *	24	25 *	24	25 *	36	11 *	38		
F	57	0 *	47	11	24	25	39	25	24	11	47	0 *	57	
G	55	0	51	38	25 *	39	53 *	39	25 *	38	51	0	55	
H	57	0 *	47	11	24	25	39	25	24	11	47	0 *	57	
I		38	11 *	36	25 *	24	25 *	24	25 *	36	11 *	37		
J		47	0	37	36	11	38	11	36	37	0	47		
K			55	0	11 *	47	51	47	11 *	0	55			
L				47	37	0 *	0	0 *	38	47				
M						57	55	57						

# Results

## 4. Full core

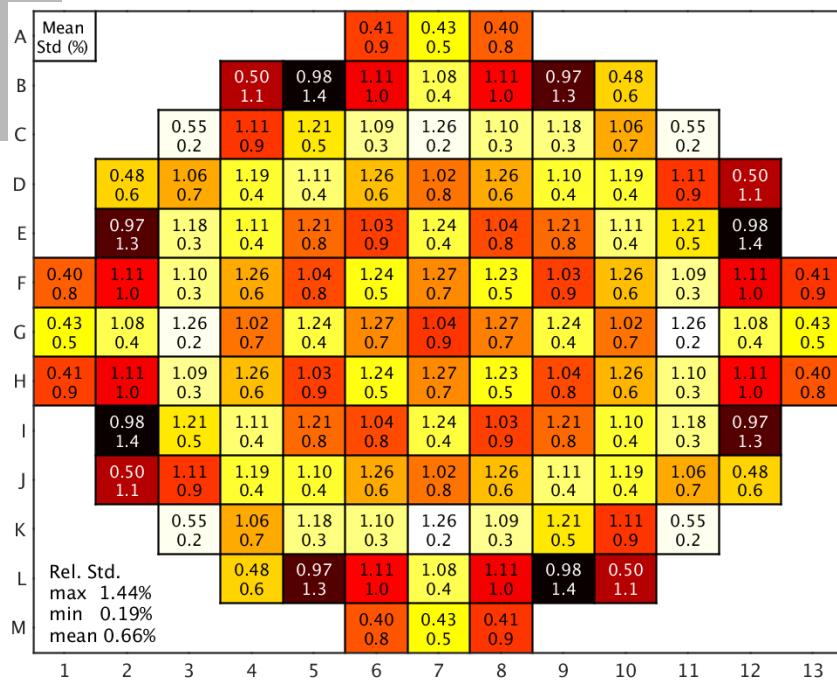
- Example with CASMO/SIMULATE,



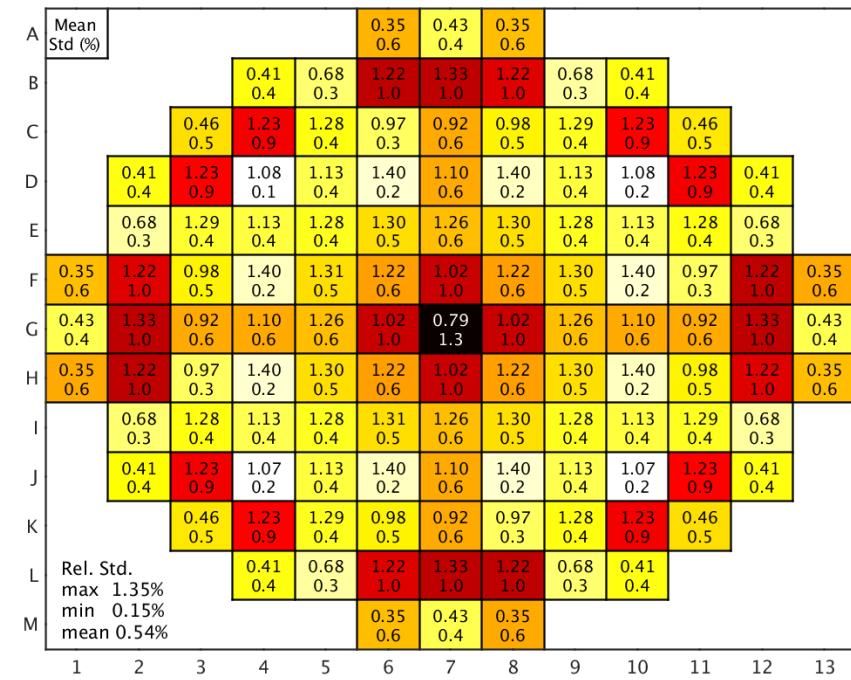
# Results

## 4. Full core

- Example with CASMO/SIMULATE,



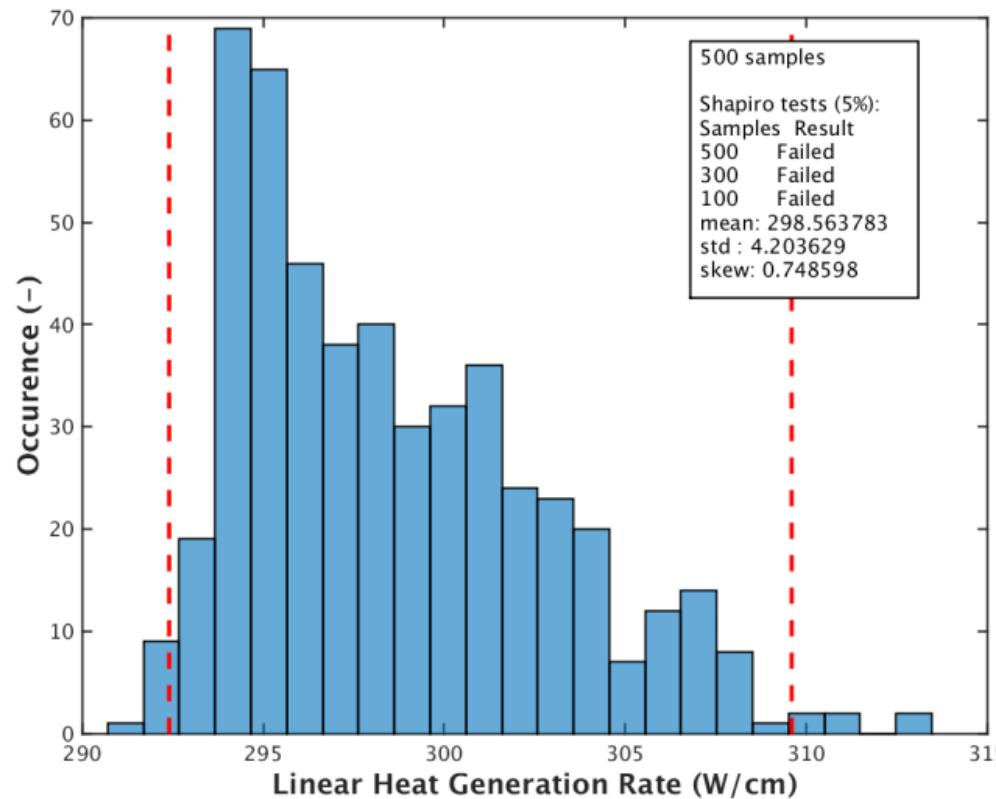
Relative radial power distributions of the MOX

Relative radial power distributions of the UO<sub>2</sub>

# Results

## 4. Full core

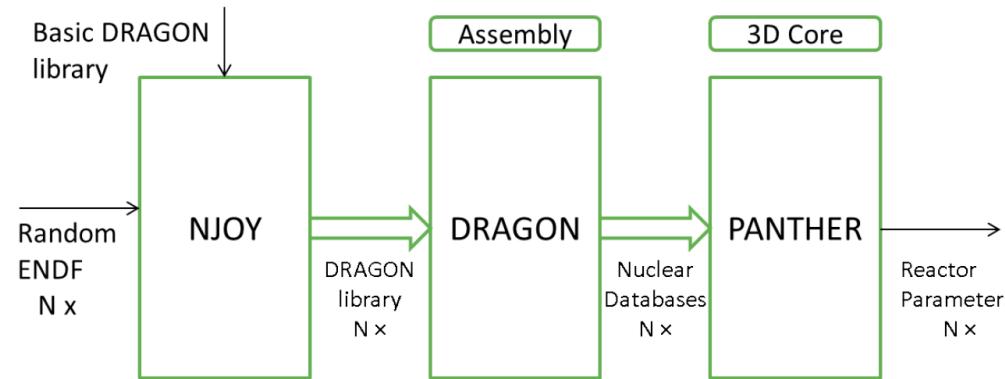
- Asymmetric distributions for safety parameters



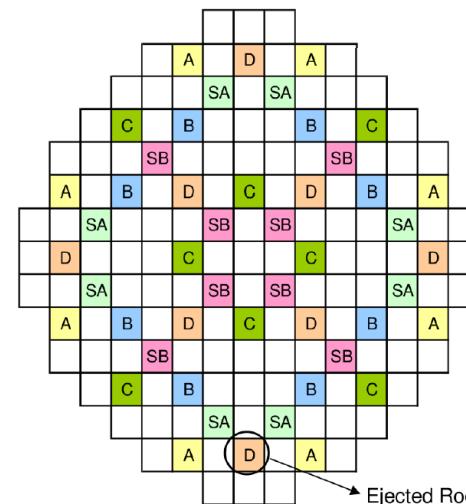
# Results

## 6. Transient

- Control Rod Ejection Accident, with ND uncertainties ( $^{235,238}\text{U}$ ,  $^{239}\text{Pu}$ , thermal scattering)



**Figure 1.** Calculation scheme for the determination of the uncertainties in the main reactor parameters due to nuclear data uncertainties.

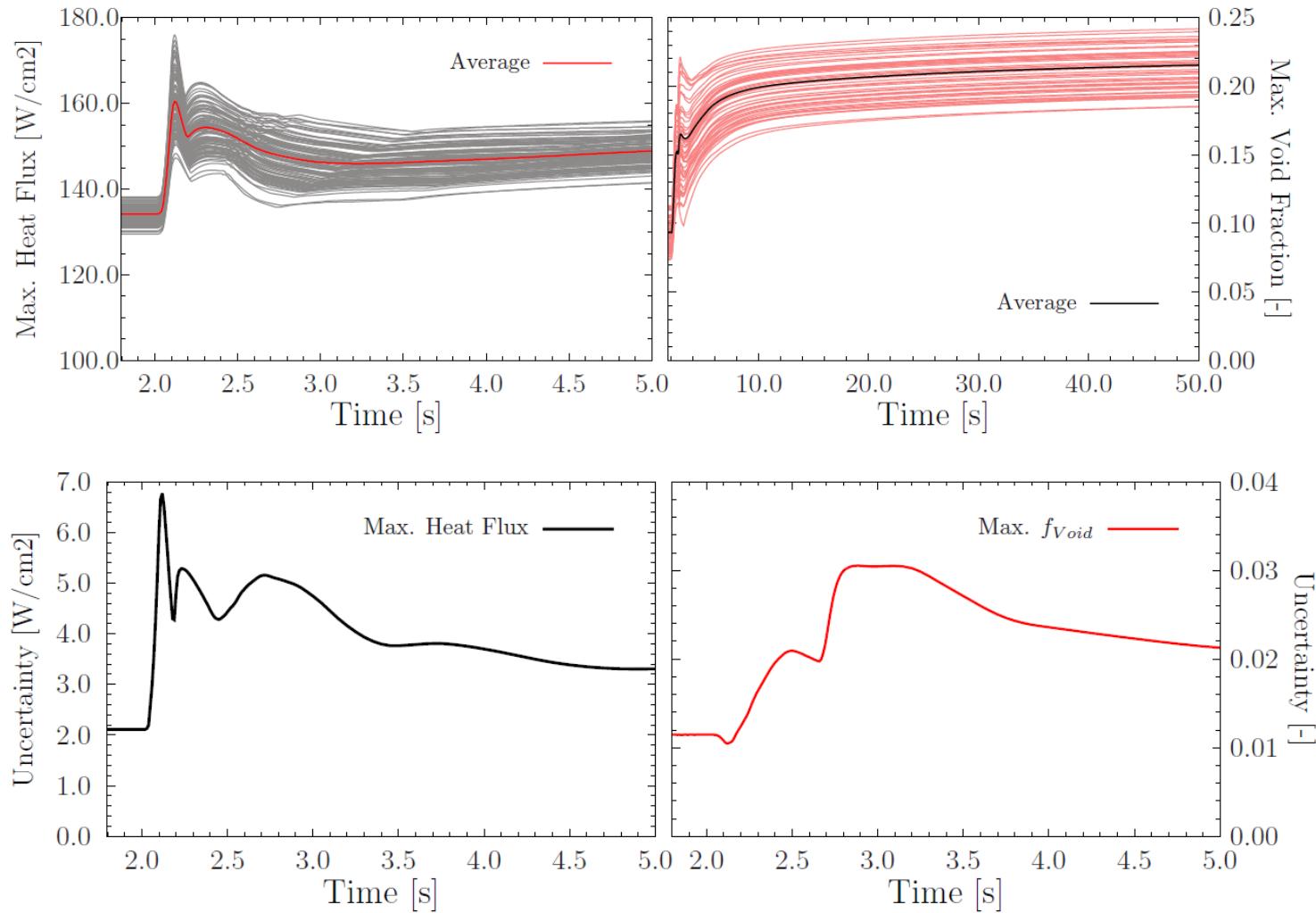


**Figure 2.** Scheme of Westinghouse core with distribution of control rod banks and position of the ejected control rod.

# Results

## 6. Transient

- Control Rod Ejection Accident, with ND uncertainties



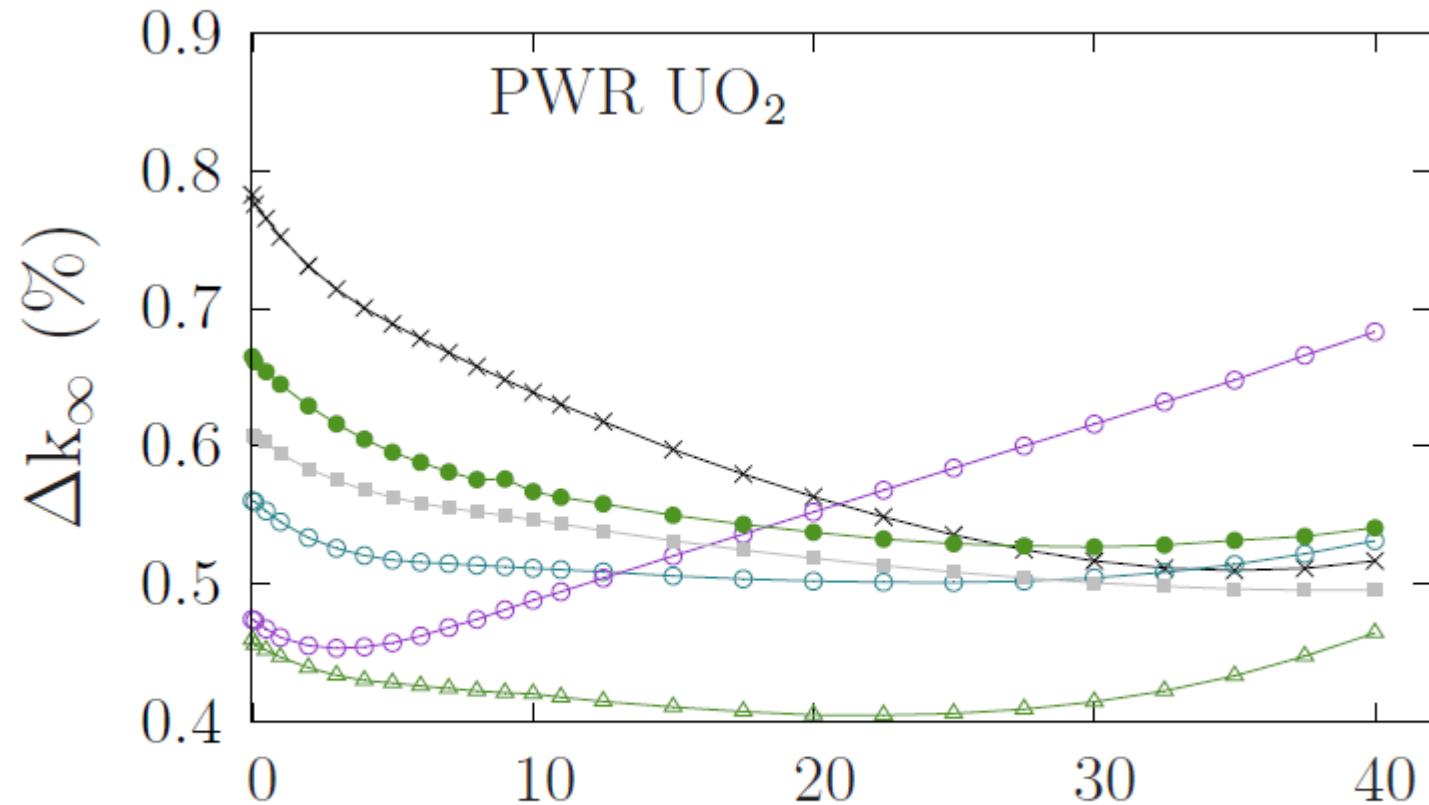
# Uncertainty from methods

*“Among different participants, given a model definition, which uncertainties do we obtain ?*

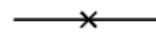
*How are the spread of uncertainties compared to the uncertainties themselves ?”*

- Uncertainties due to nuclear data are larger than from many other sources,
  - 1. Sources of nuclear data uncertainties vary: JEFF, ENDF/B, JENDL,TENDL,SCALE, in-house...
  - 2. Processing of nuclear data vary,
  - 3. Methods of uncertainty propagation vary: deterministic, Monte Carlo,
  - 4. Methods of neutron transport/depletion also vary.
- 
- This approach is then different than the UAM requirements,
  - It is close to a real-case assignment given by a third party to a TSO (Technical Support Organization).

# Uncertainty from methods



CASMO + ENDF/B-VII.1 (PSI)



Burn-up (MWd/kgU)

CASMO + SCALE-6.2 (PSI)



DRAGON + JENDL-4.0 (UU)



DRAGON + ENDF/B-VII.1 (UU)



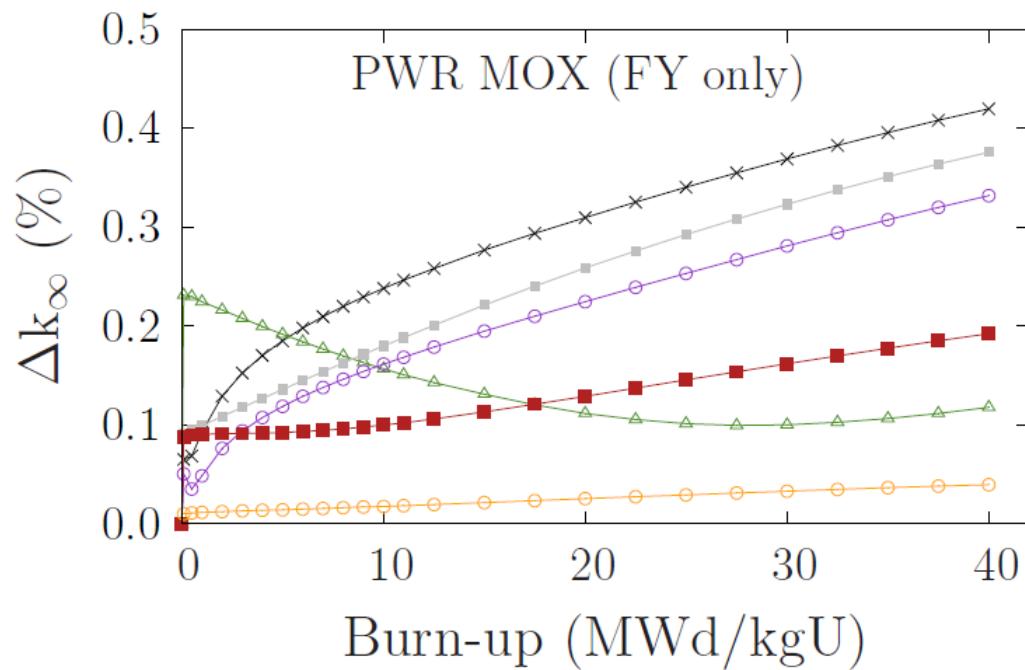
TRITON + SCALE-6.1 (GRS)



TRITON + SCALE-6.2 (UPM)

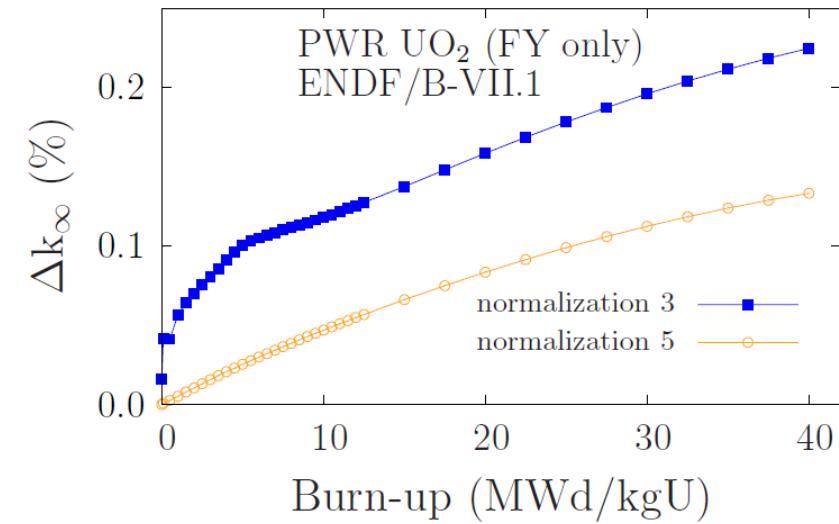


# Uncertainty from methods



GEF

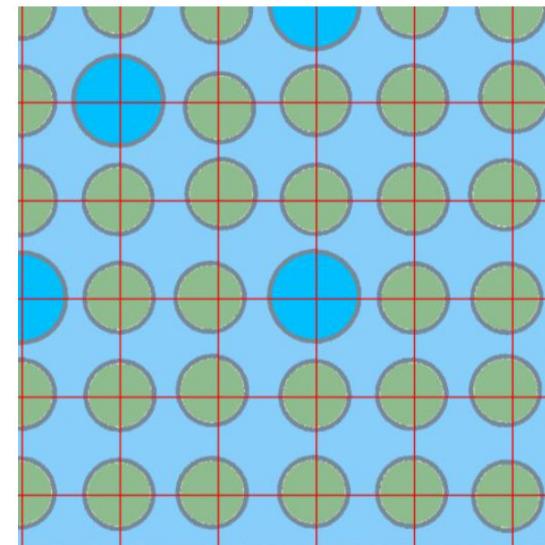
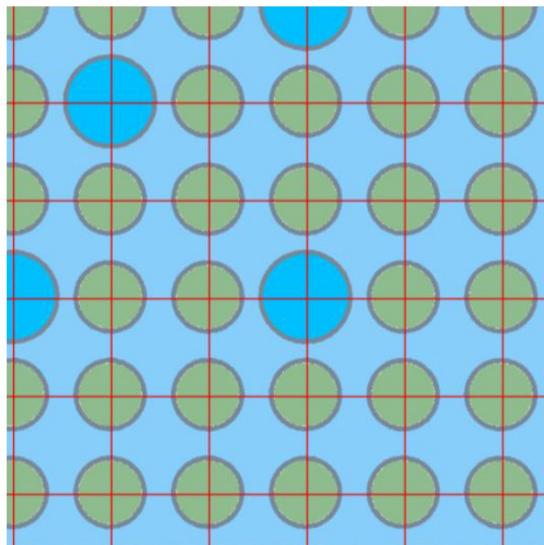
- ENDF/B-VII.1 normalization 1
- ENDF/B-VII.1 + normalization 2
- ENDF/B-VII.1 + normalization 3
- ENDF/B-VII.1 + normalization 4
- ENDF/B-VII.1 + normalization 5



- Normalization 1: mass & charge
- Normalization 2: GEF correlation
- Normalization 3: Updated GEF (see [1])
- Normalization 4:  $\sum \text{FY}=2$
- Normalization 5: SANDY

# Other Uncertainties

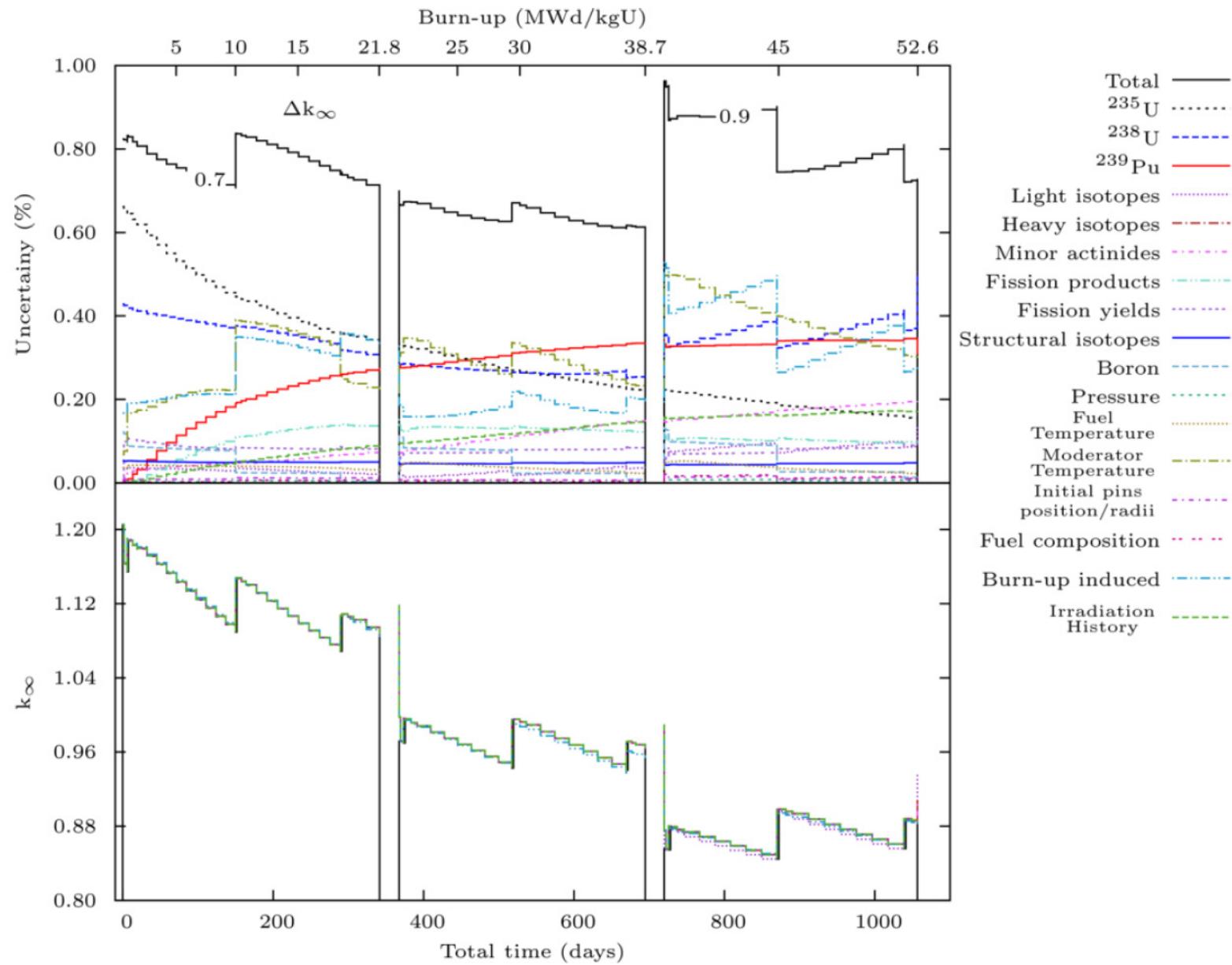
- For assembly/reactor calculations, other sources of uncertainties appear:
  - Nuclear data,
  - Reactor operating conditions,
  - Manufacturing tolerances,
  - Burnup induced technological changed,
  - ...
- All play a role for the assessment on the final quantities



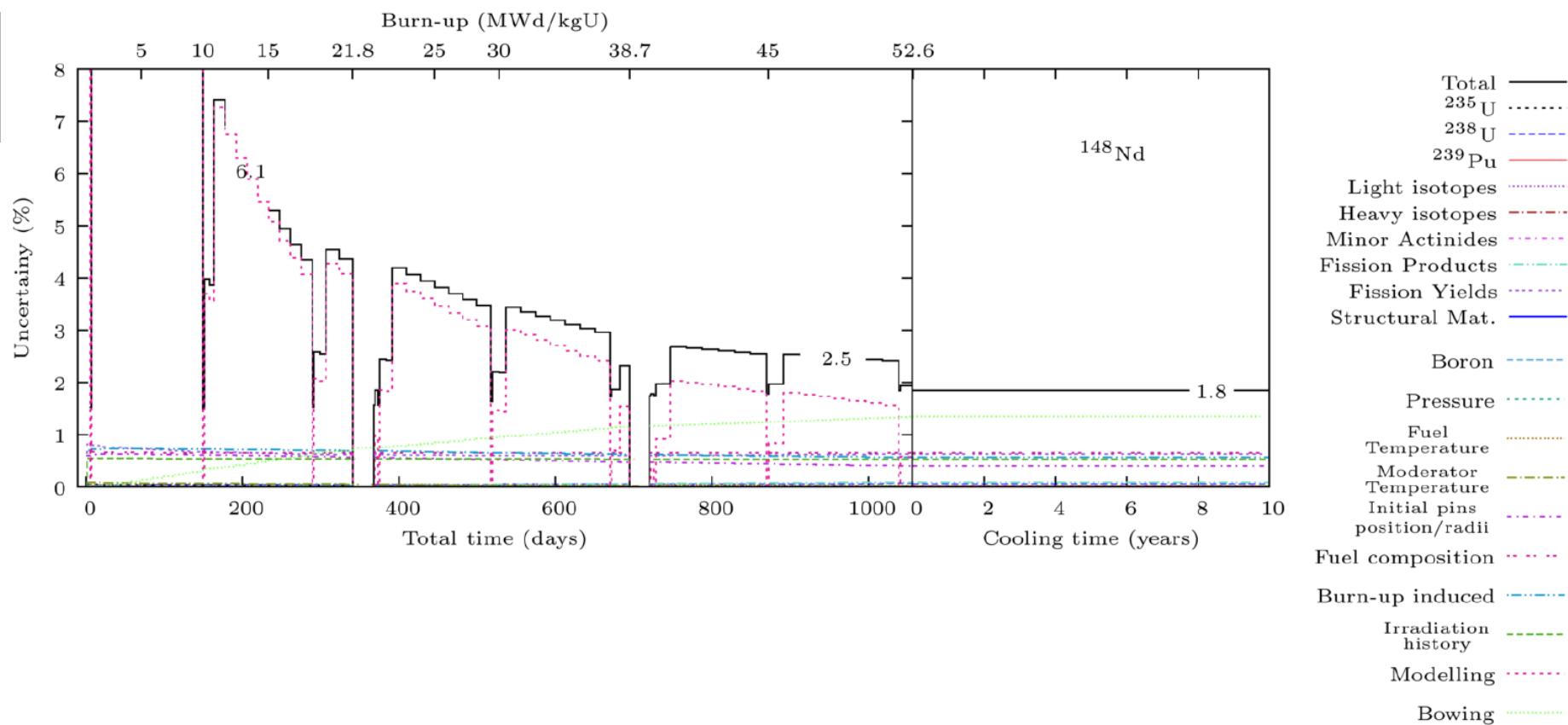
**Figure 9:**

Two random distributions of fuel pins with different enrichments and densities.  
The colors indicate different fuel pins.

# Other Uncertainties

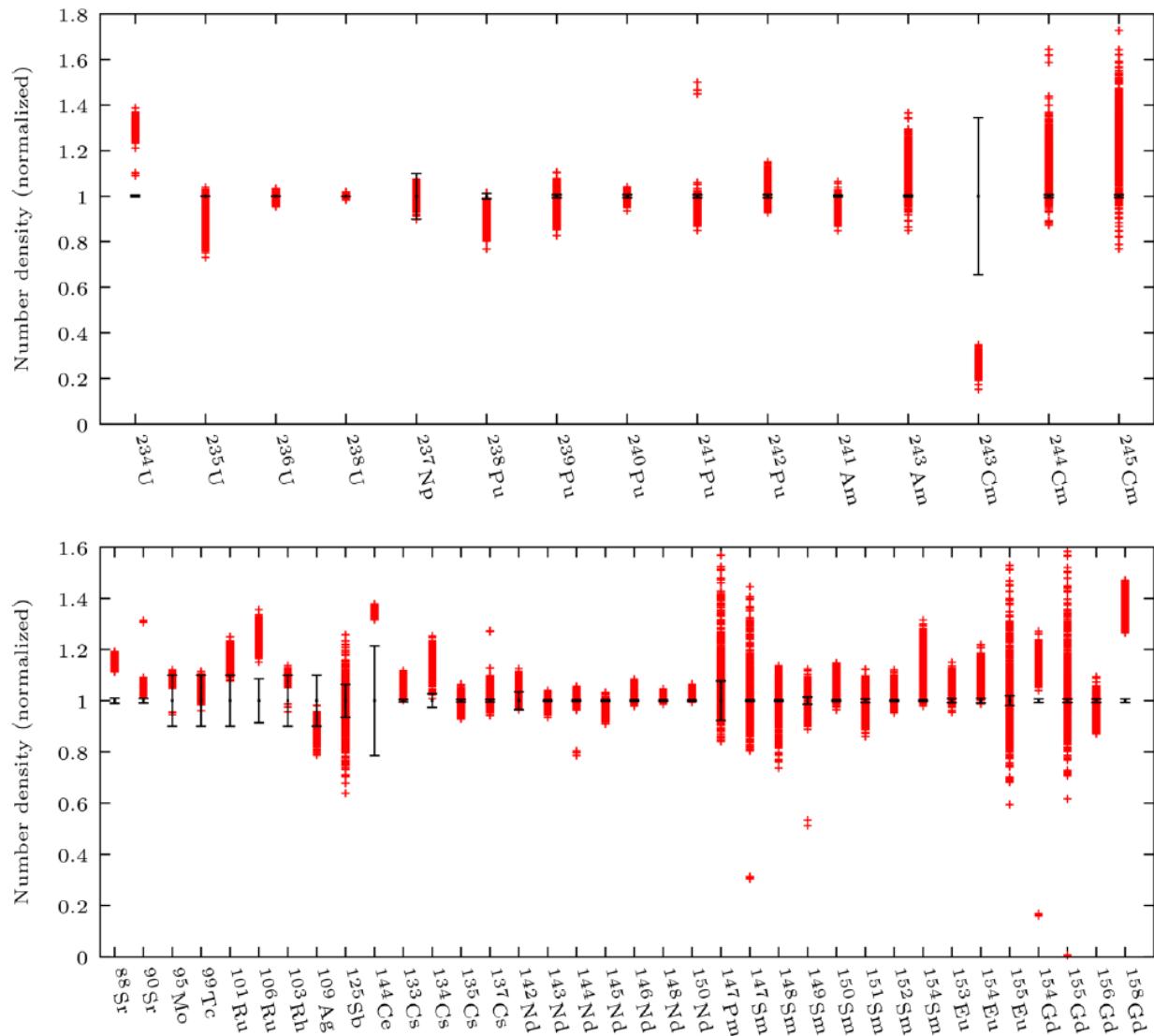


# Other Uncertainties



# Other Uncertainties

- Finally, the analysis of the total uncertainties help to explain possible differences in C/E ratios



# Conclusion

1. Nuclear data uncertainties can nowadays be propagated in large-scale systems, to any quantities
2. A necessary condition is to be able to randomly change the nuclear data (not possible if hardcoded in simulation codes).
3. Other sources of uncertainties exist
4. Finally, uncertainties should be replaced by pdf.

*The spread of uncertainties can be higher than the uncertainties themselves  
(because of methods, sources of data, codes...).*

*This puts in perspective calculated uncertainties.*

# Wir schaffen Wissen – heute für morgen

